



# TUTORIAL ON THERMAL RATING OF LINES (TB 207)

Prepared by Study Committee B2  
Advisory Group 4 – Electrical Effects  
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- Calculation of conductor temperature
  - Steady State
  - Transient
  - Abiabatic

HEAT GAIN = HEAT LOSS

$$P_j + P_M + P_S + P_i = P_c + P_r + P_w \quad (1)$$

where

$P_j$  = joule heating

$P_M$  = magnetic heating

$P_S$  = solar heating

~~$P_i$~~  = corona heating

$P_c$  = convective cooling

$P_r$  = radiative cooling

~~$P_w$~~  = evaporative cooling



## IMPORTANT FORMULAE – Ohmic Heat Loss

Ohmic Heating

$$P_i = k_i I^2 R_{dc} [1 + \alpha (T_{av} - 20)]$$

Radial Temperature Difference

$$T_c - T_s = \frac{P_T}{2\pi\lambda} \left[ \frac{1}{2} - \frac{D_1^2}{D^2 - D_2^2} \left( \ln \frac{D}{D_2} \right) \right]$$

$P_T$  = the total heat gain per unit length

$D$  = the external conductor diameter, i.e. the outer diameter

$D_2$  = the internal diameter which is the diameter of the steel core

$T_s$  = surface temperature

$T_c$  = core temperature

$\lambda$  = effective radial thermal conductivity

Forced Convective Cooling

$$P_c = \pi \lambda_f (T_s - T_a) Nu$$

$$Nu = B_1 (Re)^n$$

$$Re = \rho_r v D / \nu,$$

Effect of wind angle

$$Nu_\delta = Nu_{90} \left[ A_1 + B_2 (\sin \delta)^{m_1} \right]$$

$$A_1 = 0.42, B_2 = 0.68 \text{ and } m_1 = 1.08 \text{ for } 0^\circ < \delta < 24^\circ$$

$$A_1 = 0.42, B_2 = 0.58 \text{ and } m_1 = 0.90 \text{ for } 24^\circ < \delta < 90^\circ$$



# IMPORTANT FORMULAE – Low Convection < 0.5 mps

When the wind blows parallel to the conductor axis the Nusselt number with a wind angle of  $0^\circ$  drops to around  $0.42 Nu_{90}$ . This is due to swirling of the flow due to the stranding of the conductor.

With low wind velocity ( $V < 0.5$  m/s), however, it has been found that there is no preferred wind direction and the Nusselt number is unlikely to go below (refer section 3.1.3 for calculation of cooling at low wind speeds):

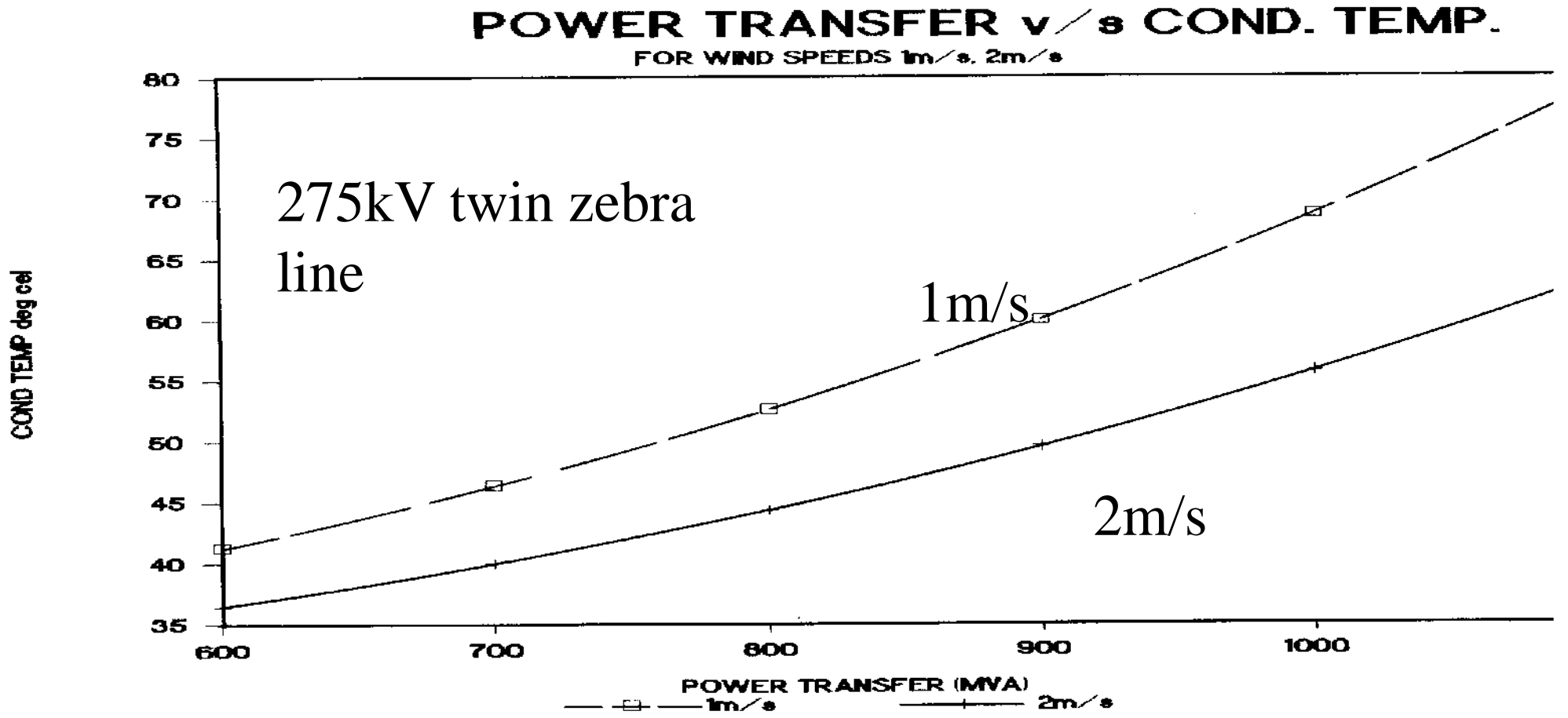
$$Nu_{cor} = 0.55 Nu_{90} \quad (15)$$

$Nu_{cor}$  is the corrected Nusselt number.

Also note that there is no preferred direction so the low wind speed is assumed to be at 45 deg.

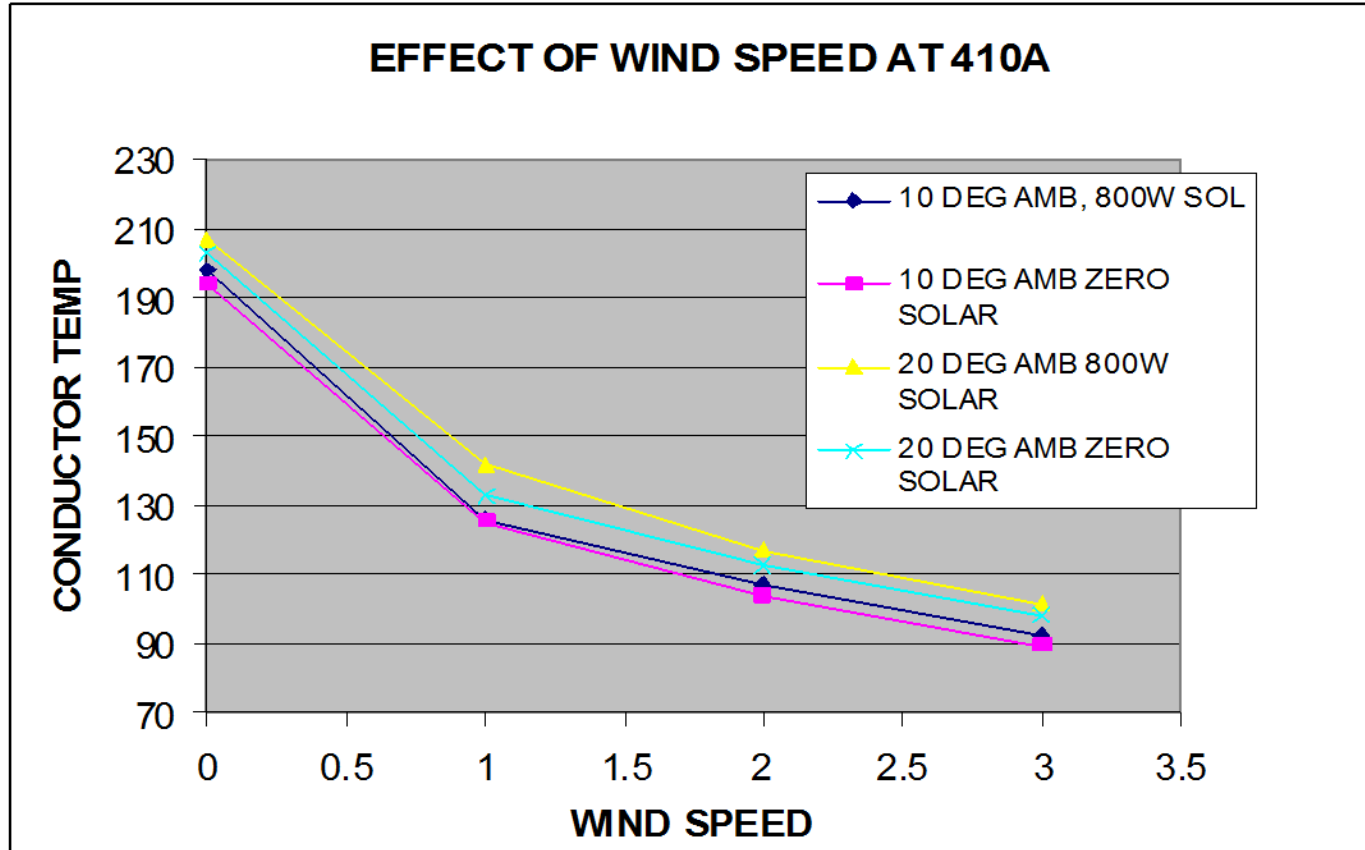
- Dependent on the diameter of conductor
- Absorptivity and emissivity
  - How dark or how shiny is the conductor?
  - Shiny conductors run hotter at high current levels.
    - Be careful on new lines with immediate high loadings
    - Conductor inserts.
- Dependent on solar radiation.
  - Global depending on direct and diffuse.
- Solar radiation less impact on high templating temperature lines with high current densities.

# Effect of templating temperature and wind





# EFFECT OF WIND SPEED



## Use of Steady State Formulae

- Determine the long term steady state rating for conductors.
- Determine the optimum templating temperature for new lines or uprating of old lines.

$$\frac{\partial T}{\partial t} = \frac{\lambda}{\gamma c} \left( \frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} \right) + \frac{q(T, r, t)}{\gamma c}$$

$$T_{av} = \frac{T_c + T_s}{2}$$

Since the mass per unit length  $m = \gamma A$  and  $q = P/A$ , where  $A$  is the cross-sectional area and  $P$  is the power per unit length,

$$mc \frac{dT_{av}}{dt} = P_J + P_M + P_S - P_r - P_c$$

$$t = \frac{-mc\theta_m}{I^2 R_{ac} + P_S} \ln \left( \frac{\theta_m - \theta}{\theta_m - \theta_1} \right)$$

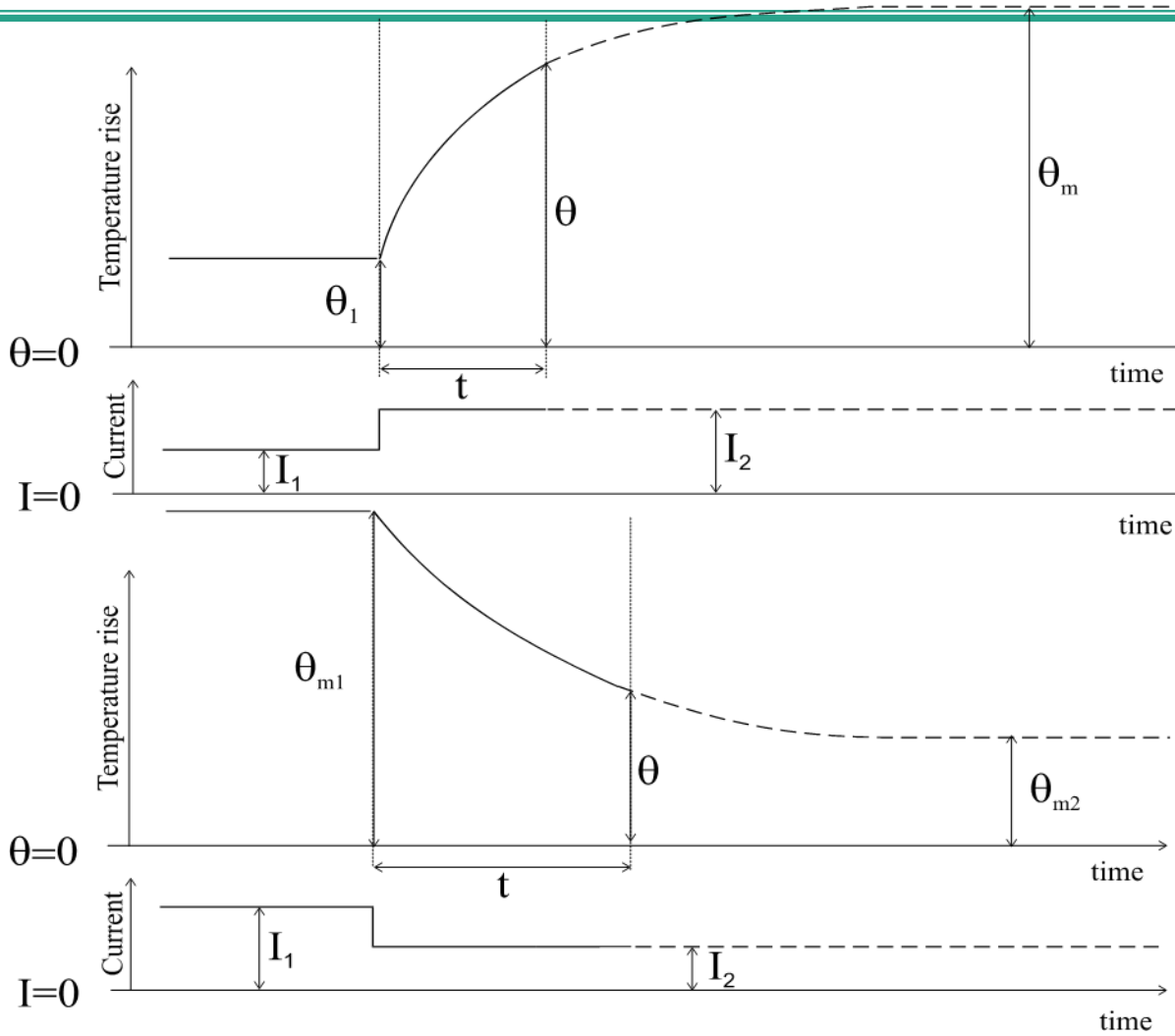
$R_{ac}$  = ac resistance per unit length at ambient temperature

$\theta$  =  $T_{av} - T_a$  = average temperature rise of conductor

$\theta_1$  =  $T_{av1} - T_a$  = initial average temperature rise of conductor at time  $t_1$

$\theta_m$  =  $T_{avm} - T_a$  = asymptotic average temperature rise of conductor

# Heating and Cooling



- The time constant is around 20 minutes.
- Wind has major effect on conductor temperature.
- Wind is variable within the time constant.
- Load is variable.
- This allows for increased real time rating to be determined.

The interval of time is calculated using equation (21):

$$dt_i = \frac{mc(\theta_i) \cdot d\theta}{P_J(\theta_i) + P_M(\theta_i) + P_S - P_C(\theta_i) - P_R(\theta_i)}$$

where  $\theta_i$  is the temperature rise at step i.

- At high templating temperatures solar radiation has minimal effect.
  - Highest temperatures occur at night.
- Steady state used for deterministic ratings and certain probabilistic ratings - templating temperature.
- Unsteady state used for Real time monitoring and certain probabilistic ratings - operational benefits.